



# Varying processing parameters in the development of slurry-based oxide bond coat for environmental barrier coatings

R. I. Webster, K. N. Lee, B. J. Puleo  
NASA Glenn Research Center, Cleveland, OH

47<sup>th</sup> International Conference and Expo on Advanced Ceramics and Coatings  
S2: Environmental Barrier Coatings II

January 26, 2023

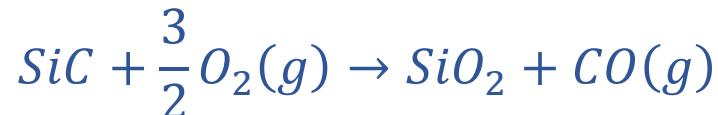
Funded by: Transformational Tools & Technologies (TTT) Project  
Hybrid Thermally Efficient Core (HyTEC) Project



# Introduction

- Silicon carbide (SiC)-based ceramic matrix composites (CMCs) are an attractive alternative to nickel-base superalloys as hot-section aircraft engine components
  - Lower density and higher operating temperature improve engine efficiency
- CMCs require an environmental barrier coating (EBC) to prevent volatilization of the protective  $\text{SiO}_2$  scale formed on SiC in a combustion environment

Oxidation



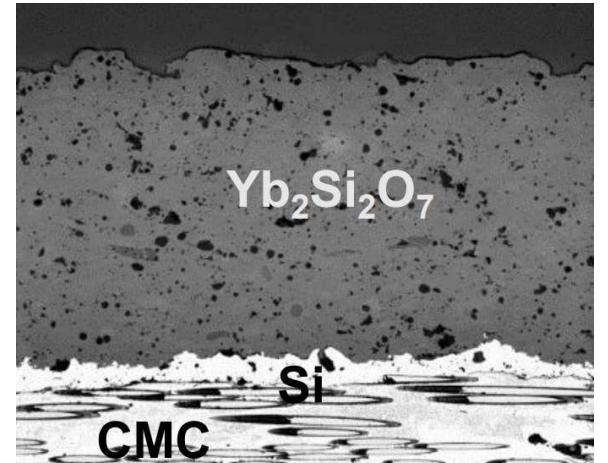
Recession





# Motivation

- Current-generation EBCs consist of a rare earth (RE) silicate ( $\text{RE}_2\text{Si}_2\text{O}_7$ ;  $\text{RE}_2\text{SiO}_5$ ) top coat and a Si bond coat
- Upper use temperature limited by melting point of Si bond coat ( $\sim 1410^\circ\text{C}$ )
  - Operating temperature of 2700°F (1482°C) desired



<https://ntrs.nasa.gov/api/citations/20180004253>

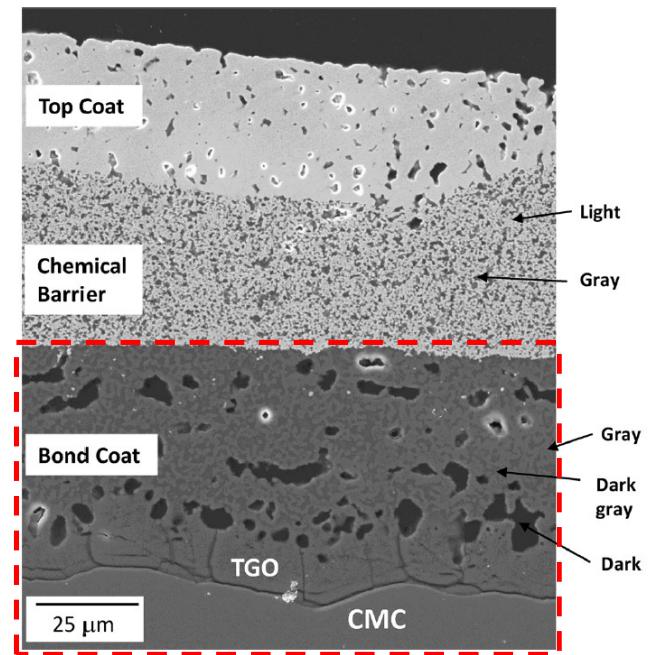


# Motivation

- A slurry-based oxide bond coat with significantly higher temperature capabilities has been developed at NASA Glenn Research Center
  - Three-layer system
  - Cycling at 1427°C in 90 vol% H<sub>2</sub>O/10 vol% O<sub>2</sub>

	Mullite	Yb <sub>2</sub> Si <sub>2</sub> O <sub>7</sub>	HfSiO <sub>4</sub>	Al <sub>2</sub> O <sub>3</sub>	Si
Top coat	0.2 – 1 wt%	balance			0 – 10 wt%
Chemical barrier			balance		10 wt%
Bond coat	balance	1.3 wt%		7	20 wt%

500 h at 1427°C; ~15 µm thick TGO



KN Lee et al., J. Eur. Ceram. Soc., 41 1639–1653 (2021).



# Objective

- Explore the effects of processing and chemistry on slurry-based oxide bond coat performance at  $\sim 1480^{\circ}\text{C}$  in a steam cycling environment

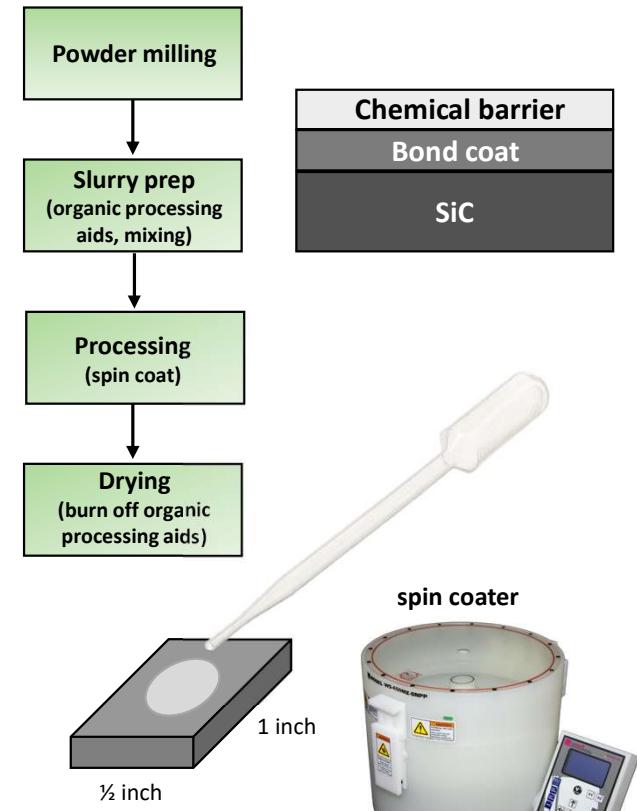


# Experimental

- Slurry processes (dip, spray, spin) provide a feasible, inexpensive, and scalable method for producing coatings
- Slurry = powder + solution (solvent + binder + dispersant)
- A bond coat (5 mil) and chemical barrier (5 mil) were deposited on Hexoloy® SA coupons via spin coating

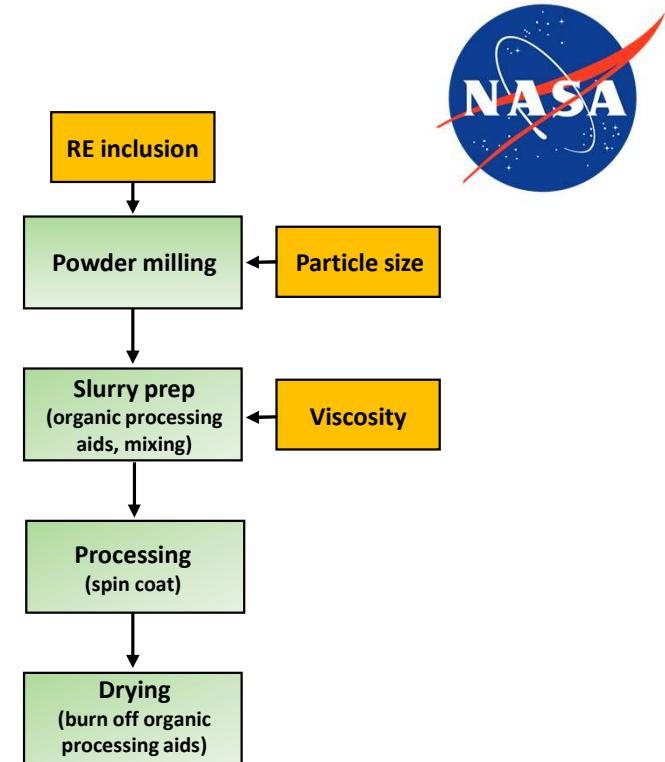
	Mullite	$RE_2Si_2O_7$	$HfSiO_4$	$Al_2O_3$	Si	SiC
<b>Chemical barrier</b>			balance		2 wt%	
<b>Bond coat</b>	balance	$\leq 1$ wt%		< 1 wt%	15 wt%	5 wt%

KN Lee, DL Waters, U.S. Patent 11325869, 10 May 2022.



# Experimental

- Bond coat variables:
  - Particle size
    - Powders prepared with 2, 3, or 5 mm diameter  $\text{ZrO}_2$  milling media
  - Viscosity
    - Slurry viscosity varied between  $\sim 10$  ("low viscosity") and 20 – 30 cP ("standard viscosity")
  - RE inclusion
    - Yb/Sc/Lu



	Mullite	$\text{RE}_2\text{Si}_2\text{O}_7$	$\text{HfSiO}_4$	$\text{Al}_2\text{O}_3$	Si	SiC
Chemical barrier			balance		2 wt%	
Bond coat	balance	$\leq 1$ wt%		< 1 wt%	15 wt%	5 wt%

KN Lee, DL Waters, U.S. Patent 11325869, 10 May 2022.

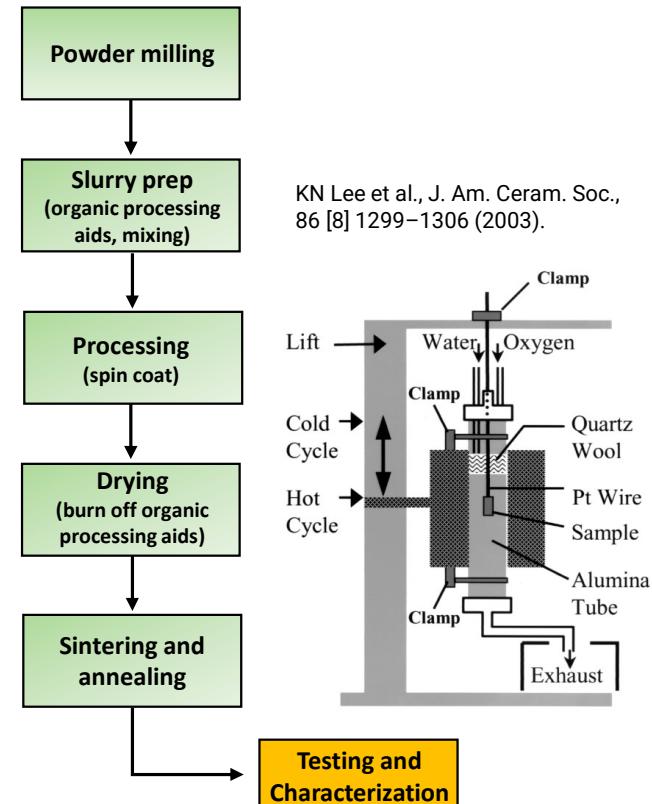


# Experimental

- Dried coupons sintered for 3 h at  $\sim 1525^{\circ}\text{C}$  and annealed for 10 h at  $\sim 1480^{\circ}\text{C}$  in a stagnant-air box furnace
- Sintered/annealed samples exposed in a steam cycling rig (1 hour hot, 30 min cool) at  $\sim 1480^{\circ}\text{C}$ 
  - 90 vol%  $\text{H}_2\text{O}$ /10 vol%  $\text{O}_2$
  - 10 cm/s gas velocity
- Coating performance evaluated macroscopically and by scanning electron microscopy (SEM)

	Mullite	$\text{RE}_2\text{Si}_2\text{O}_7$	$\text{HfSiO}_4$	$\text{Al}_2\text{O}_3$	Si	SiC
<b>Chemical barrier</b>			balance		2 wt%	
<b>Bond coat</b>	balance	$\leq 1$ wt%		< 1 wt%	15 wt%	5 wt%

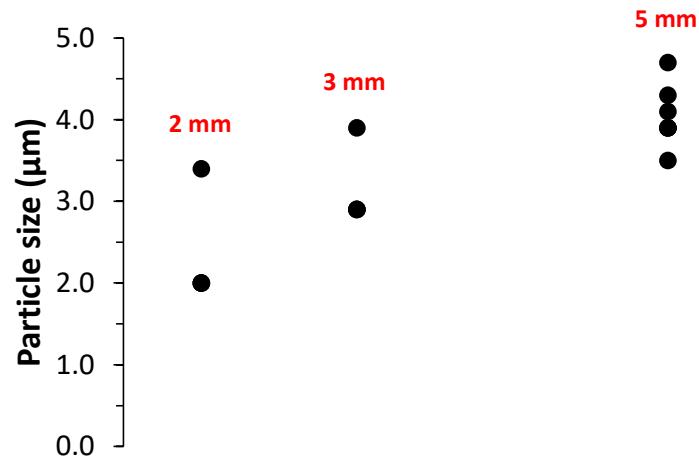
KN Lee, DL Waters, U.S. Patent 11325869, 10 May 2022.





## Results: Particle size

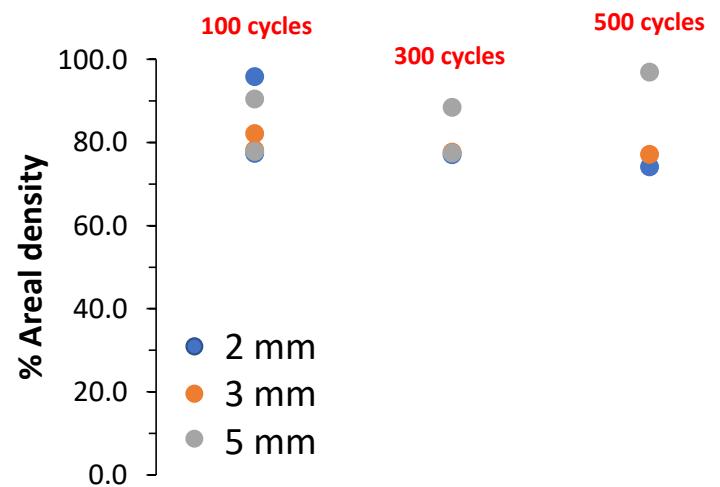
- Average particle size ranged from 2.0 to 4.7  $\mu\text{m}$
- Smaller particle size = denser bond coat?
  - $\uparrow$  density,  $\uparrow$  elastic modulus,  $\uparrow$  thermal stress during cycling





## Results: Particle size

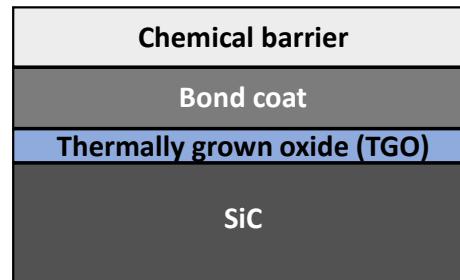
- Average particle size ranged from 2.0 to 4.7  $\mu\text{m}$
- Smaller particle size = denser bond coat?
  - $\uparrow$  density,  $\uparrow$  elastic modulus,  $\uparrow$  thermal stress during cycling
- Density not significantly different across initial particle size range investigated



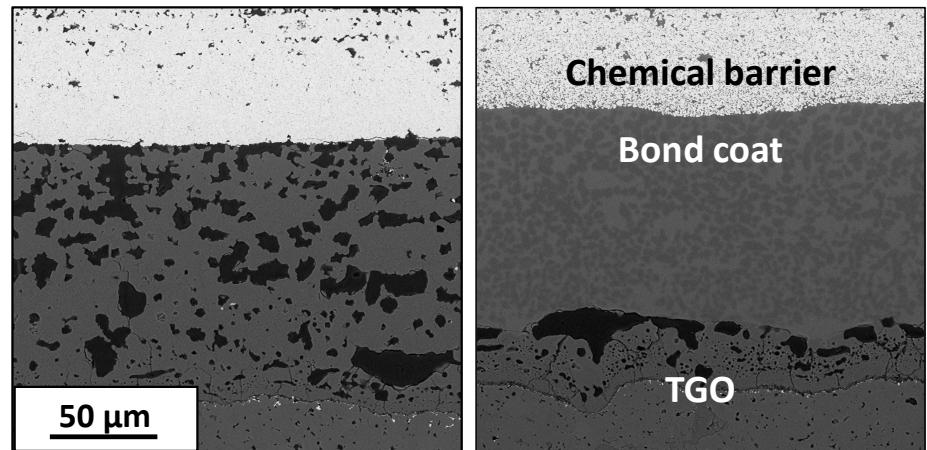


## Results: Particle size

- Average particle size ranged from 2.0 to 4.7  $\mu\text{m}$
- Smaller particle size = denser bond coat?
  - $\uparrow$  density,  $\uparrow$  elastic modulus,  $\uparrow$  thermal stress during cycling
- Density not significantly different across initial particle size range investigated
  - Differences in density likely due to other factors



Particle size = 2.0  $\mu\text{m}$ ; 500 cycles,  $\sim 1480^\circ\text{C}$



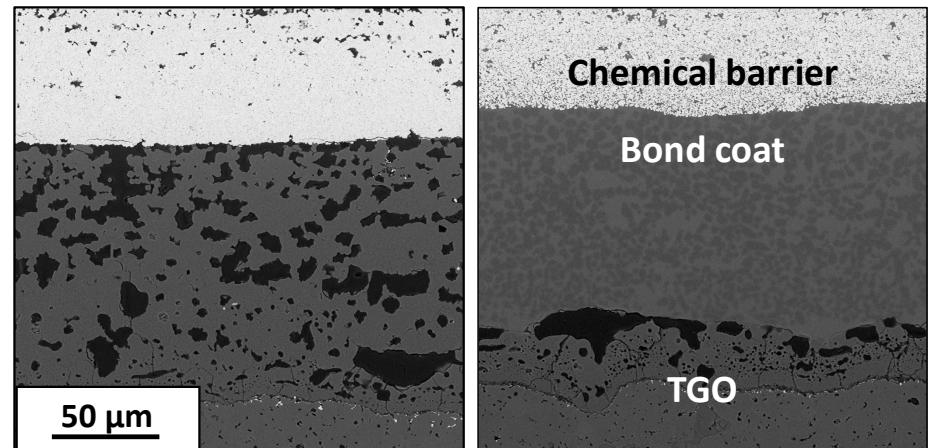


## Results: Particle size

- Average particle size ranged from 2.0 to 4.7  $\mu\text{m}$
- Smaller particle size = denser bond coat?
  - $\uparrow$  density,  $\uparrow$  elastic modulus,  $\uparrow$  thermal stress during cycling
- Density not significantly different across initial particle size range investigated
  - Differences in density likely due to other factors

No apparent trends with respect to density or performance as a function of particle size.

Particle size = 2.0  $\mu\text{m}$ ; 500 cycles,  $\sim 1480^\circ\text{C}$





## Results: Viscosity

- “Standard” viscosity = powder to solution ratio of 36/64 (wt%)
- “Low viscosity” = powder to solution ratio of 25/75 (wt%)



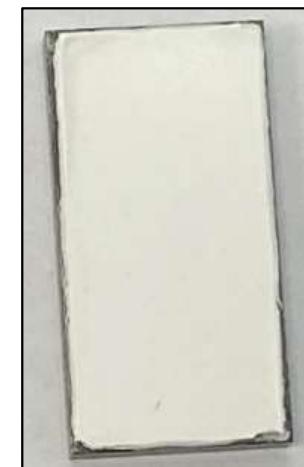
# Results: Viscosity

- “Standard” viscosity = powder to solution ratio of 36/64 (wt%)
- “Low viscosity” = powder to solution ratio of 25/75 (wt%)
- Low viscosity samples generally showed improved resistance to edge-lifting/edge effects after processing

Standard viscosity



Low viscosity



As-processed



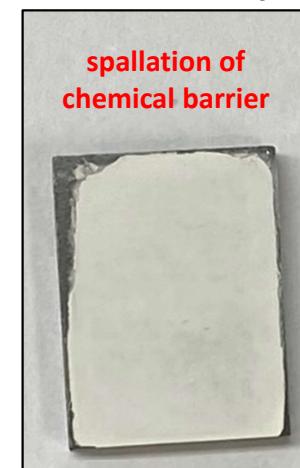
## Results: Viscosity

- Low viscosity samples generally showed improved resistance to edge-lifting/edge effects after processing
- Only minor improvements in bond coat performance in a steam cycling environment were observed across multiple samples

Standard viscosity



Low viscosity

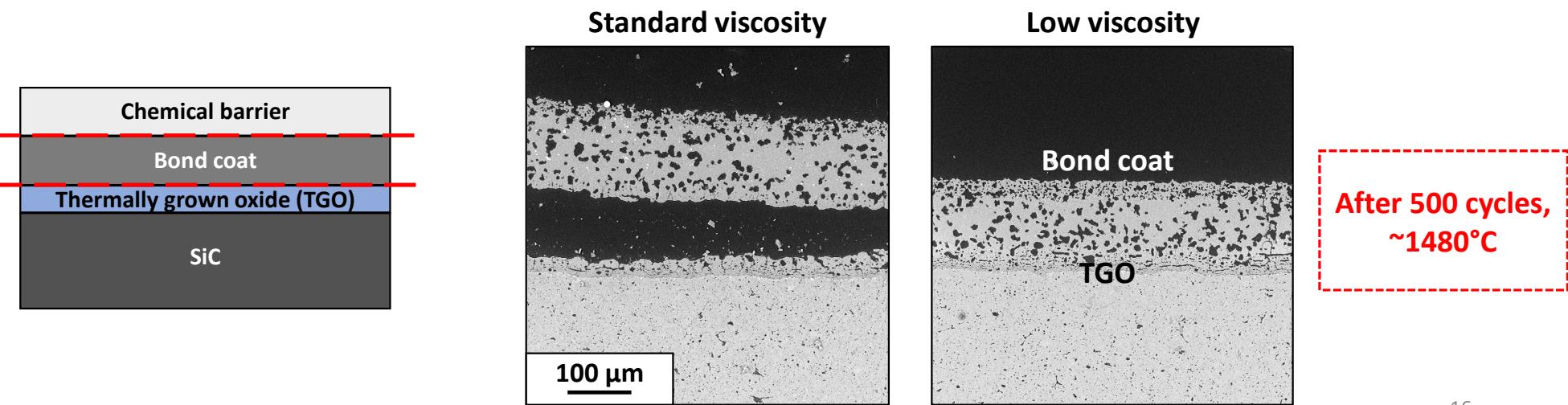


After 500 cycles,  
~1480°C



# Results: Viscosity

- Low viscosity samples generally show improved resistance to edge-lifting/edge effects after processing
- Only minor improvements in bond coat performance in a steam cycling environment were observed across multiple samples
  - No significant difference in density between standard and low viscosity samples

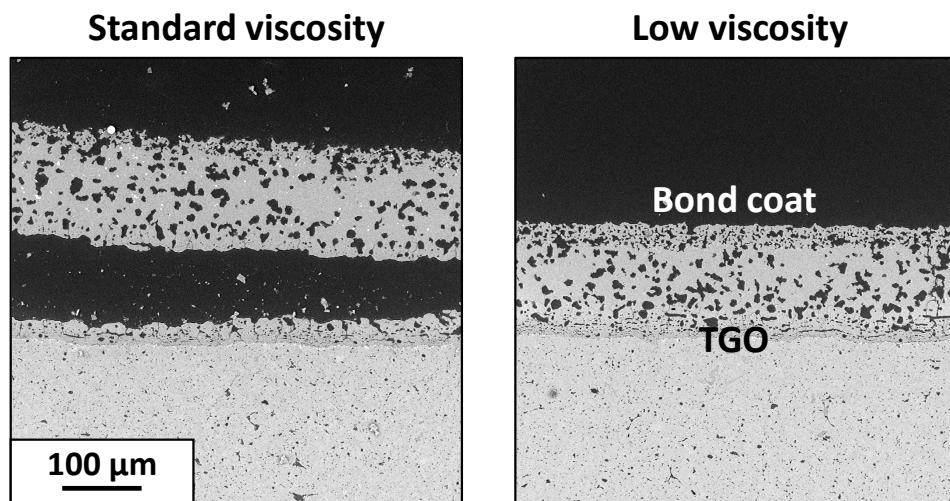




# Results: Viscosity

- Low viscosity samples generally show improved resistance to edge-lifting/edge effects after processing
- Only minor improvements in bond coat performance in a steam cycling environment were observed across multiple samples
  - No significant difference in density between standard and low viscosity samples

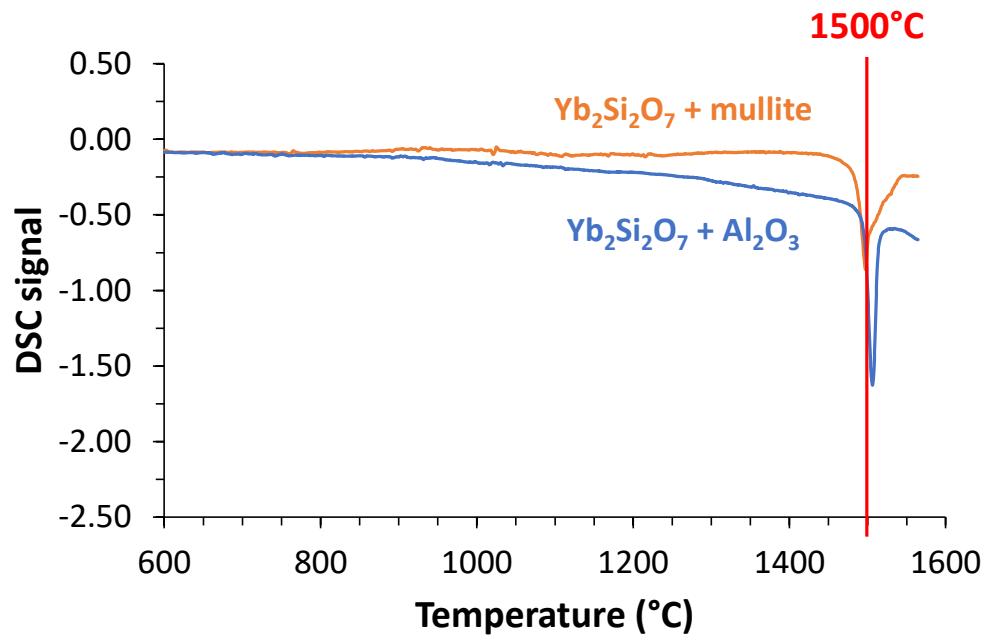
A lower viscosity slurry results in somewhat improved bond coat performance.





## Results: RE inclusion

- Substitution of Sc or Lu for Yb in  $\text{RE}_2\text{Si}_2\text{O}_7$  expected to increase the  $\text{RE}_2\text{Si}_2\text{O}_7$  + mullite/ $\text{Al}_2\text{O}_3$  eutectic temperature



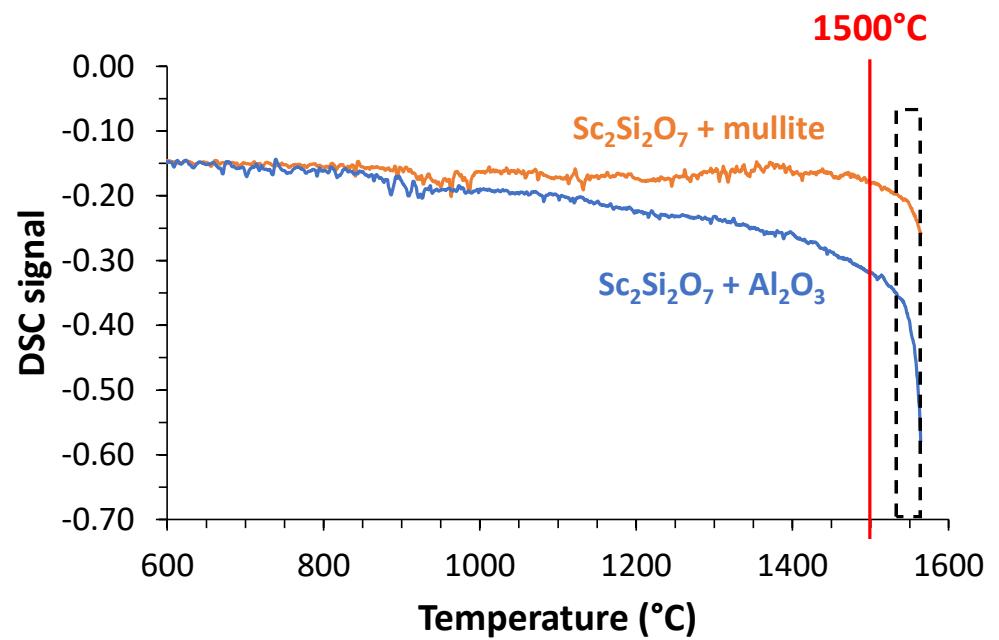
KN Lee, DL Waters, U.S. Patent 11325869, 10 May 2022.

	Mullite	$\text{RE}_2\text{Si}_2\text{O}_7$	$\text{Al}_2\text{O}_3$	Si	SiC
<b>Bond coat</b>	balance	≤ 1 wt%	< 1 wt%	15 wt%	5 wt%



## Results: RE inclusion

- Substitution of Sc or Lu for Yb in  $\text{RE}_2\text{Si}_2\text{O}_7$  expected to increase the  $\text{RE}_2\text{Si}_2\text{O}_7$  + mullite/ $\text{Al}_2\text{O}_3$  eutectic temperature



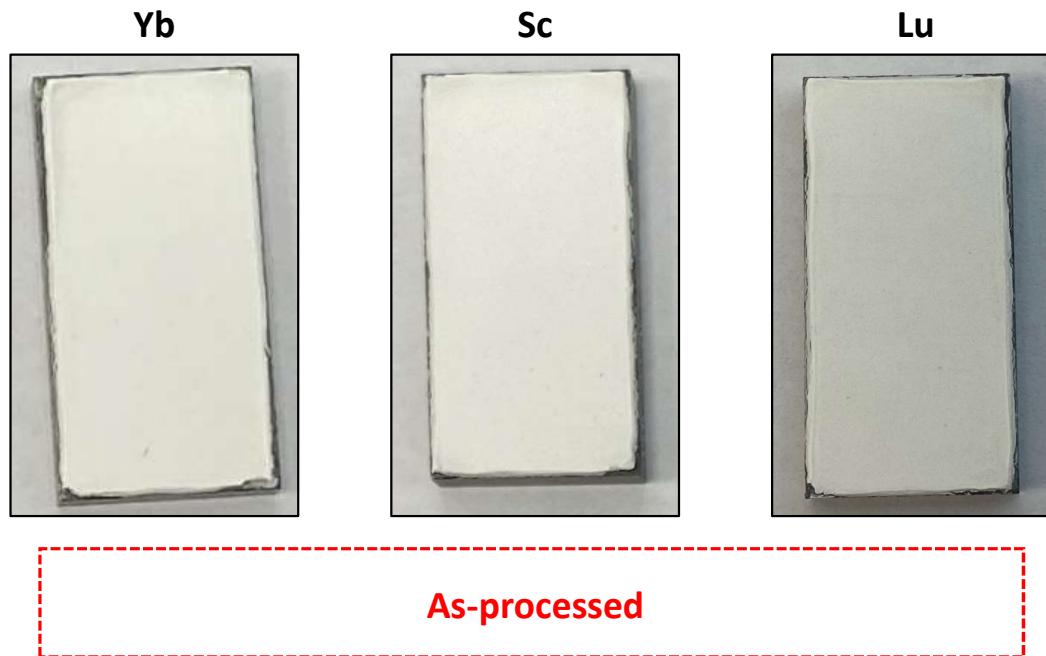
KN Lee, DL Waters, U.S. Patent 11325869, 10 May 2022.

	Mullite	$\text{RE}_2\text{Si}_2\text{O}_7$	$\text{Al}_2\text{O}_3$	Si	SiC
<b>Bond coat</b>	balance	≤ 1 wt%	< 1 wt%	15 wt%	5 wt%



## Results: RE inclusion

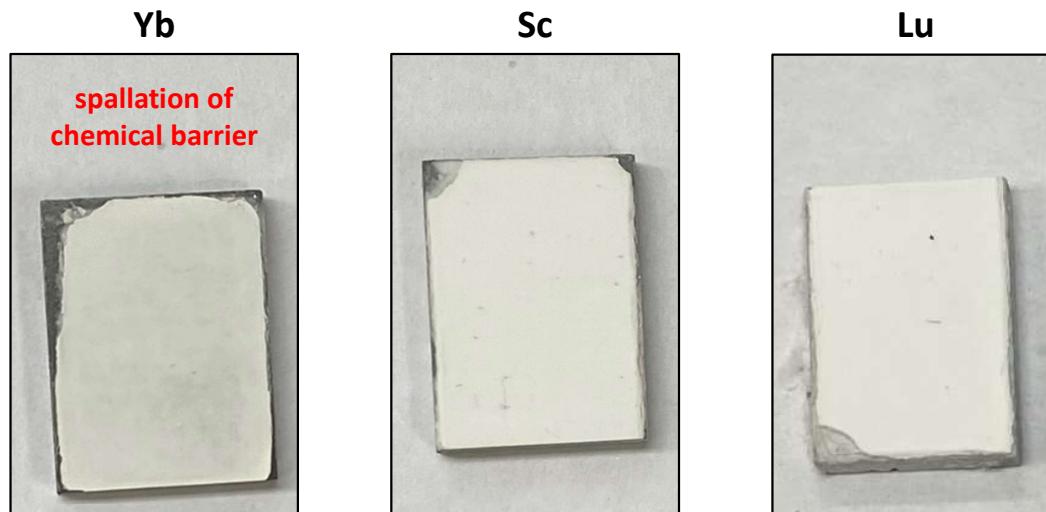
- 1:1 substitution of Sc or Lu for Yb results in improved bond coat performance
  - Slurry prepared as “low viscosity”; 5 mm milling media





## Results: RE inclusion

- 1:1 substitution of Sc or Lu for Yb results in improved bond coat performance
  - Slurry prepared as “low viscosity”; 5 mm milling media

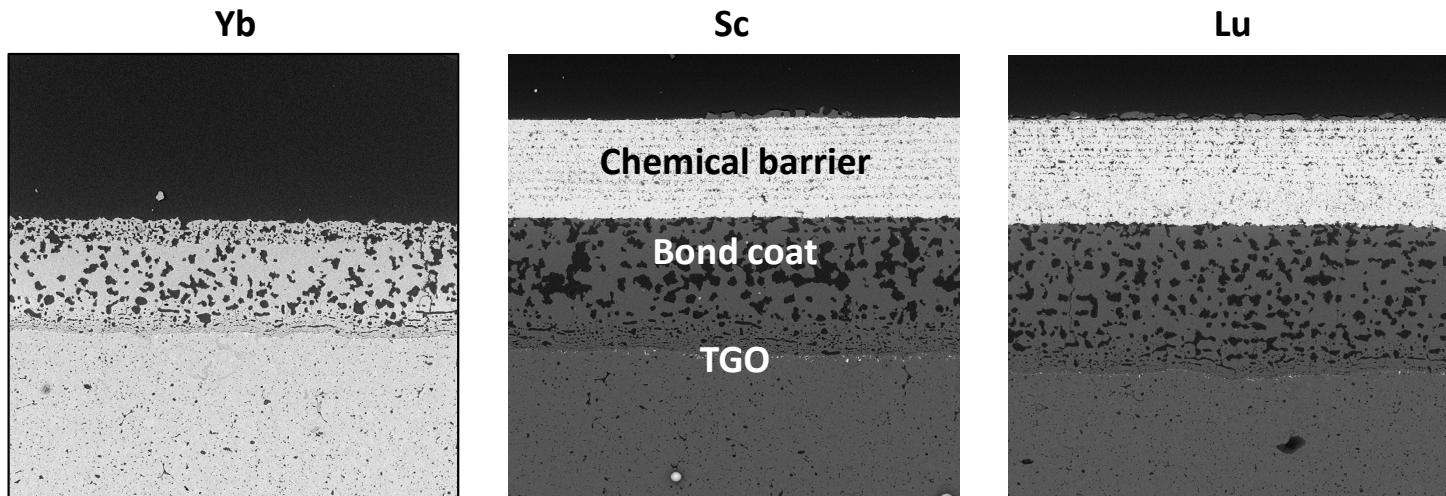


After 500 cycles,  $\sim 1480^{\circ}\text{C}$



## Results: RE inclusion

- 1:1 substitution of Sc or Lu for Yb results in improved bond coat performance
  - Slurry prepared as “low viscosity”; 5 mm milling media



After 500 cycles, ~1480°C



## Results: RE inclusion

- 1:1 substitution of Sc or Lu for Yb results in improved bond coat performance
  - Slurry prepared as “low viscosity”; 5 mm milling media
- Additional research is underway to optimize the substitution amount
  - Density  $\text{Yb}_2\text{Si}_2\text{O}_7$  = 6.15 g/cm<sup>3</sup>
  - Density  $\text{Lu}_2\text{Si}_2\text{O}_7$  = 6.249 g/cm<sup>3</sup>
  - Density  $\text{Sc}_2\text{Si}_2\text{O}_7$  = 3.396 g/cm<sup>3</sup>

Substitution of the RE in  $\text{RE}_2\text{Si}_2\text{O}_7$  has the most pronounced effect on oxide bond coat performance.



# Summary

- The effects of particle size, slurry viscosity, and RE chemistry on the performance of a slurry-based oxide bond coat in a steam cycling environment were explored



# Summary

- The effects of particle size, slurry viscosity, and RE chemistry on the performance of a slurry-based oxide bond coat in a steam cycling environment were explored
- There was no trend in bond coat performance as a function of particle size observed over the particle size range investigated



# Summary

- The effects of particle size, slurry viscosity, and RE chemistry on the performance of a slurry-based oxide bond coat in a steam cycling environment were explored
- There was no trend in bond coat performance as a function of particle size observed over the particle size range investigated
- Lowering the slurry viscosity reduced edge-lifting after processing



# Summary

- The effects of particle size, slurry viscosity, and RE chemistry on the performance of a slurry-based oxide bond coat in a steam cycling environment were explored
- There was no trend in bond coat performance as a function of particle size observed over the particle size range investigated
- Lowering the slurry viscosity reduced edge-lifting after processing
- The type of RE in  $\text{RE}_2\text{Si}_2\text{O}_7$  had the strongest effect on bond coat performance



## Future work

- The effects of particle size, slurry viscosity, and RE chemistry on the performance of a slurry-based oxide bond coat in a steam cycling environment were explored
- There was no trend in bond coat performance as a function of particle size observed over the particle size range investigated
- Lowering the slurry viscosity reduced edge-lifting after processing
- The type of RE in  $\text{RE}_2\text{Si}_2\text{O}_7$  had the strongest effect on bond coat performance
  
- Future work will explore particle size and viscosity effects after bond coat chemistry has been optimized, specifically with respect to RE inclusion
- A slurry-based,  $\text{HfO}_2$ -dominant top coat chemistry will be investigated